

**Amendments to the Claims:**

This listing of claims will replace all prior versions and listings of claims in the application:

**Listing of Claims:**

1-57. (Cancelled)

58. (Previously Presented) A bake-hardenable cold rolled steel sheet having excellent formability, comprising: in weight% , 0.003 ~ 0.005 % of C, 0.003 ~ 0.03 % of S, 0.01 ~ 0.1 % of Al, 0.02 % or less of N, 0.2 % or less of P, at least one of 0.03 ~ 0.2 % of Mn and 0.005 ~ 0.2 % of Cu, and the balance of Fe and other unavoidable impurities;

when the steel sheet comprises one of Mn and Cu, the composition of Mn, Cu, and S satisfying at least one following relationships:  $0.58 \cdot \text{Mn}/\text{S} \leq 10$  and  $1 \leq 0.5 \cdot \text{Cu}/\text{S} \leq 10$ , and

when the steel sheet comprises both Mn and Cu, the composition of Mn, Cu, and S satisfying the following relationships:  $\text{Mn} + \text{Cu} \leq 0.3$  and  $2 \leq 0.5 \cdot (\text{Mn} + \text{Cu})/\text{S} \leq 20$  ; and

the steel sheet comprising one or more precipitates selected from the group of MnS, CuS, and (Mn, Cu)S having an average size of 0.2  $\mu\text{m}$  or less.

59. (Previously Presented) A bake-hardenable cold rolled steel sheet having excellent formability, comprising: in weight%, 0.003 ~ 0.005 % of C, 0.005 ~ 0.03 % of S, 0.01 ~ 0.1 % of Al, 0.02 % or less of N, 0.2 % or less of P, 0.05 ~ 0.2 % of Mn, and the balance of Fe and other unavoidable impurities;

the composition of Mn and S satisfying the following relationship:  $0.58 \cdot \text{Mn}/\text{S} \leq 10$ ; and

the steel sheet comprising MnS precipitates having an average size of 0.2  $\mu\text{m}$  or less.

60. (Previously Presented)      The steel sheet as set forth in claim 59, wherein the steel sheet comprises 0.015 % or less of P.

61. (Previously Presented)      The steel sheet as set forth in claim 59, wherein the steel sheet comprises 0.004 % or less of N.

62. (Previously Presented)      The steel sheet as set forth in claim 59, wherein the steel sheet comprises 0.03 ~ 0.2 % of P.

63. (Previously Presented)      The steel sheet as set forth in claim 59, wherein the steel sheet further comprises at least one of 0.1 ~ 0.8 % of Si, and 0.2 ~ 1.2 % of Cr.

64. (Previously Presented)      The steel sheet as set forth in claim 59, wherein the steel sheet comprises 0.005 ~ 0.02 % of N, and 0.03 ~ 0.06 % of P.

65. (Previously Presented)      The steel sheet as set forth in claim 64, wherein a composition of Al and N satisfies the relationship:  $1 \leq 0.52 \cdot \text{Al}/\text{N} \leq 5$ .

66. (Previously Presented)      The steel sheet as set forth in claim 59, further comprising 0.01 ~ 0.2 % of Mo.

67. (Previously Presented)      The steel sheet as set forth in claim 63, further comprising 0.01 ~ 0.2 % of Mo.

68. (Previously Presented)      A bake-hardenable cold rolled steel sheet having excellent formability, comprising: in weight%, 0.003 ~ 0.005 % of C, 0.003 ~ 0.025 % of S, 0.01 ~ 0.08 % of Al, 0.02 % or less of N, 0.2 % or less of P, 0.01 ~ 0.2 % of Cu, and the balance of Fe and other unavoidable impurities;

the composition of Cu and S satisfying the following relationship:  
 $1 \leq 0.5 * \text{Cu} / \text{S} \leq 10$ ; and

the steel sheet comprising CuS precipitates having an average size of 0.1  $\mu\text{m}$  or less.

69. (Previously Presented) The steel sheet as set forth in claim 68, wherein the steel sheet comprises 0.015 % or less of P.

70. (Previously Presented) The steel sheet as set forth in claim 68, wherein the steel sheet comprises 0.004 % or less of N.

71. (Previously Presented) The steel sheet as set forth in claim 68, wherein the composition of Cu and S satisfies the relationship:  $1 \leq 0.5 * \text{Cu} / \text{S} \leq 3$ .

72. (Previously Presented) The steel sheet as set forth in claim 68, wherein the steel sheet comprises 0.03 ~ 0.2 % of P.

73. (Previously Presented) The steel sheet as set forth in claim 68, wherein the steel sheet further comprises at least one of 0.1 ~ 0.8 % of Si, and 0.2 ~ 1.2 % of Cr.

74. (Previously Presented) The steel sheet as set forth in claim 68, wherein the steel sheet comprises 0.005 ~ 0.02 % of N, and 0.03 ~ 0.06 % of P.

75. (Previously Presented) The steel sheet as set forth in claim 74, wherein a composition of Al and N satisfies the relationship:  $1 \leq 0.52 * \text{Al} / \text{N} \leq 5$ .

76. (Previously Presented) The steel sheet as set forth in claim 68, further comprising 0.01 ~ 0.2 % of Mo.

77. (Previously Presented) The steel sheet as set forth in claim 73, further comprising 0.01 ~ 0.2 % of Mo.

78. (Previously Presented) A bake-hardenable cold rolled steel sheet having excellent formability, comprising: in weight%, 0.003 ~ 0.005 % of C, 0.003 ~ 0.025 % of S, 0.01 ~ 0.08 % of Al, 0.02 % or less of N, 0.2 % or less of P, 0.03 ~ 0.2 % of Mn, 0.005 ~ 0.2 % of Cu, and the balance of Fe and other unavoidable impurities; the composition of Mn, Cu, and S satisfying the following relationships:  $Mn+Cu \leq 0.3$  and  $2 \leq 0.5*(Mn+Cu)/S \leq 20$ ; and the steel sheet comprising MnS, CuS, and (Mn, Cu)S precipitates having an average size of 0.2  $\mu m$  or less.

79. (Previously Presented) The steel sheet as set forth in claim 78, wherein the steel sheet comprises 0.015 % or less of P.

80. (Previously Presented) The steel sheet as set forth in claim 78, wherein the steel sheet comprises 0.004 % or less of N.

81. (Previously Presented) The steel sheet as set forth in claim 78, wherein the number of precipitates is  $2 \times 10^6$  or more per unit area ( $mm^2$ ).

82. (Previously Presented) The steel sheet as set forth in claim 78, wherein the composition of Mn, Cu and S satisfies the relationship:  $2 \leq 0.5*(Mn+Cu)/S \leq 7$ .

83. (Previously Presented) The steel sheet as set forth in claim 82, wherein the number of precipitates is  $2 \times 10^8$  or more per unit area ( $mm^2$ ).

84. (Previously Presented) The steel sheet as set forth in claim 78, wherein the steel sheet comprises 0.03 ~ 0.2 % of P.

85. (Previously Presented) The steel sheet as set forth in claim 78, wherein the steel sheet further comprises at least one of 0.1 ~ 0.8 % of Si, and 0.2 ~ 1.2 % of Cr.

86. (Previously Presented) The steel sheet as set forth in claim 78, wherein the steel sheet comprises 0.005 ~ 0.02 % of N, and 0.03 ~ 0.06 % of P.

87. (Previously Presented) The steel sheet as set forth in claim 86, wherein a composition of Al and N satisfies the relationship:  $1 \leq 0.52 \cdot \text{Al}/\text{N} \leq 5$ .

88. (Previously Presented) The steel sheet as set forth in claim 78, further comprising 0.01 ~ 0.2 % of Mo.

89. (Previously Presented) The steel sheet as set forth in claim 85, further comprising 0.01 ~ 0.2 % of Mo.

90. (Previously Presented) A method of manufacturing a bake-hardenable cold rolled steel sheet having excellent formability, comprising the steps of:

hot-rolling a steel slab with finish rolling at an  $\text{Ar}_3$  transformation temperature or more to provide a hot rolled steel sheet, after reheating the steel slab to a temperature of 1,100 °C or more,

the steel slab comprising: in weight%, 0.003 ~ 0.005 % of C, 0.005 ~ 0.03 % of S, 0.01 ~ 0.1 % of Al, 0.02 % or less of N, 0.2 % or less of P, 0.05 ~ 0.2 % of Mn, and the balance of Fe and other unavoidable impurities; and

the composition of Mn and S satisfying the following relationship:  
 $0.58 \cdot \text{Mn}/\text{S} \leq 10$  ;

cooling the steel sheet at a speed of 200 °C /min or more;

winding the cooled steel sheet at a temperature of 700 °C or less and then cold rolling the steel sheet; and

continuous annealing the cold rolled steel sheet so as to obtain the cold rolled steel sheet comprising MnS precipitates having an average size of 0.2  $\mu\text{m}$  or less.

91. (Previously Presented) The method as set forth in claim 90, wherein the steel slab comprises 0.015 % or less of P.

92. (Previously Presented) The method as set forth in claim 90, wherein the steel slab comprises 0.004 % or less of N.

93. (Previously Presented) The method as set forth in claim 90, wherein the steel slab comprises 0.03 ~ 0.2 % of P.

94. (Previously Presented) The method as set forth in claim 90, wherein the steel slab further comprises at least one of 0.1 ~ 0.8 % of Si, and 0.2 ~ 1.2 % of Cr.

95. (Previously Presented) The method as set forth in claim 90, wherein the steel slab comprises 0.005 ~ 0.02 % of N, and 0.03 ~ 0.06 % of P.

96. (Previously Presented) The method as set forth in claim 95, wherein a composition of Al and N satisfies the relationship:  $1 \leq 0.52 \cdot \text{Al}/\text{N} \leq 5$ .

97. (Previously Presented) The steel sheet as set forth in claim 90, wherein the steel slab further comprises 0.01 ~ 0.2 % of Mo.

98. (Previously Presented) The steel sheet as set forth in claim 94, wherein the steel slab further comprises 0.01 ~ 0.2 % of Mo.

99. (Currently Amended) A method of manufacturing a bake-hardenable cold rolled steel sheet having excellent formability, comprising the steps of:

hot-rolling a steel slab with finish rolling at an  $Ar_3$  transformation temperature or more to provide a hot rolled steel sheet, after reheating the steel slab to a temperature of 1,100 °C or more,

the steel slab comprising: in weight% , 0.003 ~ 0.005 % of C, 0.003 ~ 0.025 % of S, 0.01 ~ 0.08 % of Al, 0.02 % or less of N, 0.2 % or less of P, 0.01 ~ 0.2 % of Cu , the balance of Fe and other unavoidable impurities and,

the composition of Cu and S satisfying the following relationship:  $1 \leq 0.5 \cdot Cu/S \leq 10$  in terms of weight; cooling the steel sheet at a speed of 300 °C/min or more;

winding the cooled steel sheet at a temperature of 700 °C or less and then cold rolling the steel sheet; and

continuous annealing the cold rolled steel sheet so as to obtain the cold rolled steel sheet comprising  $GnS$  CuS precipitates having an average size of 0.2  $\mu m$  or less.

100. (Previously Presented) The method as set forth in claim 99, wherein the steel slab comprises 0.015 % or less of P.

101. (Previously Presented) The method as set forth in claim 99, wherein the steel slab comprises 0.004 % or less of N.

102. (Previously Presented) The method as set forth in claim 99, wherein the composition of Cu and S satisfies the relationship:  $1 \leq 0.5 \cdot Cu/S \leq 3$ .

103. (Previously Presented) The method as set forth in claim 99, wherein the steel slab comprises 0.03 ~ 0.2 % of P.

104. (Previously Presented) The method as set forth in claim 99, wherein the steel slab further comprises at least one of 0.1 ~ 0.8 % of Si, and 0.2 ~ 1.2 % of Cr.

105. (Previously Presented) The method as set forth in claim 99, wherein the steel slab comprises 0.005 ~ 0.02 % of N, and 0.03 ~ 0.06 % of P.

106. (Previously Presented) The method as set forth in claim 105, wherein a composition of Al and N satisfies the relationship:  $1 \leq 0.52 \cdot \text{Al}/\text{N} \leq 5$ .

107. ((Previously Presented) The method as set forth in claim 99, wherein the steel slab further comprises 0.01 ~ 0.2 % of Mo.

108. (Previously Presented) The method as set forth in claim 104, wherein the steel slab further comprises 0.01 ~ 0.2 % of Mo.

109. (Previously Presented) A method of manufacturing a bake-hardenable cold rolled steel sheet having excellent formability, comprising the steps of:

hot-rolling a steel slab with finish rolling at an  $A_{r3}$  transformation temperature or more to provide a hot rolled steel sheet, after reheating the steel slab to a temperature of 1,100 °C or more,

the steel slab comprising: in weight%, 0.003 ~ 0.005 % of C, 0.003 ~ 0.025 % of S, 0.01 ~ 0.08 % of Al, 0.02 % or less of N, 0.2 % or less of P, 0.03 ~ 0.2 % of Mn, 0.005 ~ 0.2 % of Cu, and the balance of Fe and other unavoidable impurities and,

the composition of Mn, Cu, and S satisfying the following relationships:  
 $\text{Mn} + \text{Cu} \leq 0.3$  and  $2 \leq 0.5 \cdot (\text{Mn} + \text{Cu})/\text{S} \leq 20$ ;

cooling the steel sheet at a speed of 300 °C/min or more;



winding the cooled steel sheet at a temperature of 700 °C or less and then cold rolling the steel sheet; and

continuous annealing the cold rolled steel sheet so as to obtain the cold rolled steel sheet comprising MnS, CuS, (Mn,Cu)S precipitates having an average size of 0.2  $\mu\text{m}$  or less.

110. (Previously Presented) The method as set forth in claim 109, wherein the steel slab comprises 0.015 % or less of P.

111. (Previously Presented) The method as set forth in claim 109, wherein the steel slab comprises 0.004 % or less of N.

112. (Previously Presented) The method as set forth in claim 109, wherein the number of precipitates is  $2 \times 10^6$  or more per unit area ( $\text{mm}^2$ ).

113. (Previously Presented) The method as set forth in claim 109, wherein the composition of Mn, Cu and S satisfies the relationship:  $2 \leq 0.5 \cdot (\text{Mn} + \text{Cu}) / \text{S} \leq 7$ .

114. (Previously Presented) The method as set forth in claim 113, wherein the number of precipitates is  $2 \times 10^8$  or more per unit area ( $\text{mm}^2$ ).

115. (Previously Presented) The method as set forth in claim 109, wherein the steel slab comprises 0.03 ~ 0.2 % of P.

116. (Previously Presented) The method as set forth in claim 109, wherein the steel slab further comprises at least one of 0.1 ~ 0.8 % of Si, and 0.2 ~ 1.2 % of Cr.

117. (Previously Presented) The method as set forth in claim 109, wherein the steel slab comprises 0.005 ~ 0.02 % of N, and 0.03 ~ 0.06 % of P.

118. (Previously Presented) The method as set forth in claim 117, wherein a composition of Al and N satisfies the relationship:  $1 \leq 0.52 \cdot \text{Al}/\text{N} \leq 5$ .

119. (Previously Presented) The method as set forth in claim 109, wherein the steel slab further comprises 0.01 ~ 0.2 % of Mo.

120. (Previously Presented) The method as set forth in claim 116, wherein the steel slab further comprises 0.01 ~ 0.2 % of Mo.